## Table 1-T-100 : Cooling and Dehumidifying **Heat Load Estimate Form**

Job Na	me					
Addres						
	s Used for					
		- 0~	Γ <b>+</b> ν	_	Cu	
Size  Ft.	x	= sq	.ı-t.X		Cu.	
Γί.						
Item	Area of			Factor	Btu /	
		Temp.			Hour	
	Glass	T				
	Glass		X			
<del>                                     </del>	Glass	Sq. Ft. x	X			
<del>                                     </del>	Glass	Sq. Ft. x	X X			
SkyLiak		Sq. Ft. x	X			
Sky Ligh	AND TRAIN	•		ND BOOE		
JULAN	Wall	1		ND KOOF		
-	Wall	Sq. Ft. x	X			
-	Wall	Sq. Ft. x	X			
-	Wall	Sq. Ft. x	X			
-		Sq. Ft. x	X			
Roof Su	Wall	Sq. Ft. x	X			
Roof Su Roof Sh		· ·	X		-++	
	aded IN GAIN EX	Sq. Ft. x	S AND	POOF	-++	
All Glass				KUUF		
			X			
Partition	1	Sq. Ft. x	X			
Ceiling		Sq. Ft. x	X			
Floor	INICII TO ATI	Sq. Ft. x	X TOIDE A	in.		
	INFILTRATIO					
Infiltration		Cfm x °F				
Outside				X 1.08		
Danala	INTERNAL HEAT					
People People						
Power		H.P. / KW				
Lights			x 1.08			
Appliand		OENOIDI E I	IFAT	Х		
ROOM SENSIBLE HEAT						
Supply Supply						
Duct		Duct				
Heat Ga		Leak Loss S		A.T.		
L L	FFECTIVE			Al		
India. C		LATENT H	EAI	0.00		
Infiltration		gr/b x		0.68		
Outside	Air cfm x	gr/b x	BF X	0.68		
People		People x			-++	
Steam	<b>-</b> -	Lb / hr x 1080			-++	
Appliances, Etc.					-++	
Vapor Train					-++	
Room Latent Heat Sub Total						
Supply Duct						
EFFECTIVE ROOM LATENT HEAT						
EFFECTIVE ROOM TOTAL HEAT						
Sensible: Cfm x 0f x (1-BF) x 1.08						
Latent: cfm x gr / lb x (1-BF) x 0.68						
Grand Total Heat Sub Total						
Return		Return				
Duct		Duct	H.P.	% %		

Heat Gain%	Leak Loss		
TONS = GRAND TOTAL HEAT*			

Heat Gain% Leak Loss					
TONS = GRAND TOTAL HEAT*					
Local	Time	Peak Load			
DB	WB	%RH	DP	Gr/L	b
	xxx	xxx	XX		
nditions	D	B WI	В	%RI	Н
People x VENTILATION cfm Person					
x cfm. Ver	cfi ntilation	m / Sq. t	t. =		-
				_	
x	CR	M / DOOF	₹ =		
Foot v		ofm / Ft	_		
_ reet x		_ CIIII / FL			-
SENSIBLE HEAT FACTOR AND APPARATUS DEWPOINT					
$\frac{\textit{Eff.room sens.Heat}}{\textit{Eff.room total heat}} = \phantom{aaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaaa$					
Indicated adp°F Selected adp°F					
(1 – BF) (Room Temp. ADP = Dehumidified rise					
Room Sensible Heat Dobumidified ofm					
1.08 x Dehumidified rise NOTES					
	nditions  Local DB  Inditions  RS - PEC X - X - X - X - X - X - X - X - X - X -	Local Time  DB WB  XXX  INDICATE SET OF SERVING SET	Local Time Peak Load  DB WB %RH    XXX XXX   XXX   XXX   Peach   XXX   X	Local Time Peak Local Sum  DB WB %RH DP    XXX XXX XXX XX   Noditions DB WB    Ex VENTILATION   Cfm Person     X Cfm / Sq. ft. =   Cfm. Ventilation     RS - PEOPLE X CFM / PERSO   X CRM / DOOR =   Feet x Cfm / Ft =   Feet x Cfm / Ft =   HEAT FACTOR AND APPARATU DEWPOINT     Sens Heat Factor (ESH	Local Time

## **Psychrometric Formulae**

(6)

# A. AIR MIXING EQUATIONS (Outdoor and Return Air)

$$t_m = \frac{(cfm_{0a} \times t_{0a}) + (cfm_{ra} \times t_{rm})}{cfm_{0a}} \dots$$
 (1)

$$h_m = \frac{(cfm_{0a} \times h_{0a}) + (cfm_{ra} \times h_{rm})}{cfm_{sa}}$$
 (2)

$$W_m = \frac{(cfm_{0a} \times W_{oa}) + (cfm_{ra} \times h_{rm})}{cfm_{sa}}$$
(3)

#### C. SENSIBLE HEAT FACTOR EQUATIONS

$$RSHF = \frac{RSH}{RSH + RLH} = \frac{RSH}{RTH}$$
 (25)

$$ESHF = \frac{ERSH}{RSH + ERLH} = \frac{ERSH}{ERTH}$$
 (26)

GSHF = 
$$\frac{TSH}{TSH+TLH} = \frac{TSH}{GTH}$$
 (27)

#### D. BYPASS FACTOR EQUATIONS

#### B. COOLING LOAD EQUATIONS

$$ERSH = RSH + (BF) (OASH) + RSHS^*$$
 (4)

$$ERLH = RLH + (BF) (OALH) + RLHS^*$$
 (5)

TSH = 
$$RSH + OASH + RSHS^*$$
 (7)

$$TLH = RLH + OALH + RLHS^*$$
 (8)

$$GTH = TSH + TLH + GTHS^*$$
 (9)

RSH = 
$$1.08 \times cfm_{sa} \times (t_{rm} - t_{sa})$$
 (10)

RLH = 
$$0.68 \text{ x crm}_{sa} \text{ x } (W_{rm} - W_{sa})$$
 (11)

RTH = 
$$4.45 \text{ x crm}_{sa} \text{ x } (h_{rm} - h_{as})$$
 (12)

$$RTH = RSH + RLH$$
 (13)

OASH = 
$$1.08 \text{ x cfm}_{oa} \text{ x } (t_{oa} - t_{rm})$$
 (14)

OALH = 
$$0.68 \times cfm_{oa} \times (W_{oa} - W_{rm})$$
 (15)

OATH = 
$$4.45 \text{ x cfm}_{oa} \text{ x } (h_{oa} - h_{rm})$$
 (16)

$$OATH = OASH + OALH$$
 (17)

$$(BF)(OATH) = (BF)(OASH) + (BF)(OALH)$$
 (18)

ERSH = 
$$1.08 \times cfm_{da} \times (t_{rm} - t_{adp}) (1-BF)$$
 (19)

ERLH = 
$$0.68 \times cfm_{da} \pm \times (W_{rm} - W_{adp}) (1-BF)$$
 (20)

ERTH = 
$$4.45 \times cfm_{da} \pm x (h_{rm} - h_{adp}) (1-BF)$$
 (21)

TSH = 1.08 x cfm<sub>da</sub> 
$$x (t_{edp} - t_{idp})^{**}$$
 (22)

TLH = 
$$0.68 \times cfm_{da} \pm x (W_{ea} - W_{la})^{**}$$
 (23)

GTH = 
$$4.45 \times x \times cfm_{da} x \times (h_{ea} - h_{la})^{**}$$
 (24)

# $BF = \frac{t_{ldb} - t_{adp}}{t_{edb} - t_{adp}} : (1 - BF) = \frac{t_{edb} - t_{ldp}}{t_{edb} - t_{adp}}$ (28)

$$BF = \frac{W_{la} - W_{adp}}{W_{ea} - W_{adp}} : (1 - BF) = \frac{W_{ea} - W_{la}}{W_{ea} - W_{adp}}$$
 (29)

$$\mathsf{BF} = \frac{h_{la} - h_{adp}}{h_{ea} - h_{adp}} : (1 - BF) = \frac{h_{ea} - h_{la}}{h_{ea} - h_{adp}}$$
(30)

# E. TEMPERATURE EQUATIONS AT APPARATUS

$$t_{edb} ** = \frac{(cfm_{oa} \times t_{oa}) + (cfm_{ra} \times t_{rm})}{cfm_{sa} \ddagger}$$
 (31)

$$t_{ldb} = t_{adp} + BF \ t_{edb} = t_{adp} \tag{32}$$

 $t_{edb}{}^{\star\star}$  and  $t_{lwb}$  correspond to the calculated values of  $h_{ea}$  and  $h_{la}$  on the psychrometric chart.

$$h_{ea} ** = \frac{(cfm_{oa} \times h_{oa}) + (cfm_{ra} \times h_{rm})}{cfm_{sa} \ddagger}$$
(33)

$$h_{ldb} = ht_{adp} + BF (h_{ea} = h_{adp})$$
 (34)

#### F. TEMPERATURE EQUATIONS FOR SUPPLY AIR

$$t_{sa} = t_{rm} - \frac{RSH}{1.08 (cfm_{sa} \ddagger)}$$
 (35)

## Psychrometric Formulae (Contd...)

### **G. AIR QUANTITY EQUATIONS**

$$cfm_{da} = \frac{ERSH}{1.08 \times (1-BF) (t_{rm} - t_{adp})}$$
 (36)

$$cfm_{da} = \frac{ERLH}{0.68 \times (1-BF) (W_{rm} - W_{adp})}$$
(37)

$$cfm_{da} = \frac{ERTH}{4.45 \times (1-BF) (h_{rm} - h_{adp})}$$
 (38)

$$cfm_{da} \ddagger = \frac{TSH}{1.08 \times (t_{edp} - t_{ldp})} \tag{39}$$

$$cfm_{da} \ddagger = \frac{TLH}{0.68 \times (W_{ea} - W_{la})} \tag{40}$$

$$cfm_{da} \ddagger = \frac{GTH}{4.45 \times (h_{ea} - h_{la})}$$
 (41)

$$cfm_{sa} = \frac{RSH}{1.08 \times (t_{rm} - t_{sa})} \tag{42}$$

$$cfm_{sa} = \frac{RLH}{0.68 \times (W_{rm} - W_{sa})} \tag{43}$$

$$cfm_{da} = \frac{RTH}{4.45 \times (h_{rm} - h_{SO})} \tag{44}$$

$$cfm_{ba} = cfm_{sa} - cfm_{da} (44)$$

Note:  $cfm_{da}$  will be less than  $cfm_{sa}$  only when air is physically bypassed around the conditioning apparatus.

$$cfm_{sa} = cfm_{oa} - cfm_{ra} (45)$$

$$1.08 = 0.244 \times \frac{60}{13.5}$$

Where 0.244 = Specific heat of moist air at 70 F db and 50% rh, Btu / (deg F) (lb dry air).

60 = min./hr

13.5 = specific volume of moist air at 70 F db and 50% rh

$$0.68 = \frac{60}{13.5} \times \frac{1076}{7000}$$

Where 60 = min./hr

13.5 = Specific volume of moist air at 70 F db and 50% rh

1076 = average heat removal required to condense one pound of water vapor from the room air.

7000 = grains per pound

$$4.45 = \frac{60}{13.5}$$

Where 60 = min./hr

13.5 = Specific volume of moist air at 70 F db and 50% rh

\* RSHS, RLHS and GTHS are supplementary loads due to duct heat gain, duct leakage loss, fan and pump horsepower gains, etc. To simplify the various examples, these supplementary loads have not been used in the calculations. However, in actual practice, these supplementary loads should be used where appropriate.

 $\pm$ When no air is to be physically bypassed around the conditioning apparatus,  $cfm_{da}=cfm_{sa}$ 

\*\* When  $t_m$ , Wm and  $h_m$  are equal to the entering conditions at the cooling apparatus, they may be substituted for  $t_{edp}$   $W_{ea}$  and  $h_{ea}$  respectively.

# **ABBREVIATIONS**

# **SYMBOLS**

Adp	apparatus dewpoint		
BF	bypass factor	cfm <sub>ba</sub>	bypassed air quantity around apparatus
(BF) (OALH)	bypassed coutdoor air latent heat	cfm <sub>da</sub>	dehumidified air quantity
(BF) (OASH)	bypassed outdoor air sensible heat	crm <sub>ba</sub>	outdoor air quantity
But/hr	British thermal units per hour	cfm <sub>ba</sub>	return air quantity
	·	cfm <sub>sa</sub>	supply air quantity
Cfm	cubic feet per minute	h	specific enthalpy
db	dry-bulb	$h_{adp}$	apparatus dewpoint enthalpy
dp	dewpoint	h <sub>es</sub>	effective surface temperature enthalpy
ERLH	effective room latent heat	h <sub>ea</sub>	entering air enthalpy
ERSH	effective room sensible heat	h <sub>ia</sub>	leaving air enthalpy
ERTH	effective room total heat	h <sub>m</sub>	mixture of outdoor and return air enthalpy
ESHF	effective sensible heat factor	h <sub>oa</sub>	outdoor air enthalpy
		h <sub>ra</sub>	room air enthalpy
F	Fahrenhelt degrees	h <sub>sa</sub>	supply air enthalpy
tpm	feet per minute	t	temperature
gpm	gallons per minute	$t_{\sf adp}$	apparatus dewpoint temperature
gr/lb	grains per pound	$t_{edb}$	entering dry-bulb temperature
GSHF	grand sensible heat factor	t <sub>es</sub>	effective surface temperature
GTHS	grand total heat supplement	$t_{\text{ew}}$	entering water temperature
OALH	Outdoor air latent heat	$t_{\sf ewb}$	entering wet-bulb temperature
OASH	Outdoor air sensible heat	t <sub>ldb</sub>	leaving dry-bulb temperature
OATH	Outdoor air total heat	t <sub>iwb</sub>	leaving wet-club temperature
rh	relative humidity	t <sub>m</sub>	mixture of outdoor and return air dry-bulb
RLH	room latent heat		temperature
RLHS	room latent heat supliment	$t_{oa}$	outdoor air dry-bulb temperature
RSH	room sensible heat	$t_{im}$	room dry-bulb temperature
RSHF	room sensible heat factor	$t_{sa}$	supply air dry-bulb temperature
RSHS	room sensible heat supplement	W	moisture content or specific humidity
RTH	room total heat	$W_{adp}$	apparatus dewpoint moisture content
Sat EH	saturation efficiency of spray	$W_{ea}$	entering air moisture content
SHF	sensible heat factor	$W_{es}$	effective surface temperature moisture
TLH	total latent heat		content
RSH	total sensible heat	W <sub>la</sub>	leaving air moisture content
w b	wet bulb	$W_{m}$	mixture of outdoor and return air moisture content
		$W_{oa}$	outdoor air moisture content
		$W_{m}$	room moisture content
		$W_{sa}$	supply air moisture content